## Highway/Traffic/Transportation Engineering

Classifications of highways

1. Principal arterials
2. Minor arterials
3. Major collectors
4. Minor collectors
5. Local roads and streets

Design speed
-selected speed to determine the various geometric features of the roadway

Table. Minimum Design Speed for Rural Collector Roads

| Type of <br> Terrain | Design Speed (kph) for Specified Design Volume (Vehicles / <br> day) |  |  |
| :--- | :--- | :--- | :--- |
|  | $0-400$ | 400 to 2000 | Over 2000 |
| Level | 64.39 | 80.49 | 96.59 |
| Rolling | 48.29 | 64.39 | 80.49 |
| Mountainous | 32.20 | 48.29 | 64.39 |

## Glossary

Design speed
-selected speed to determine the various geometric features of the roadway
Design vehicle
-vehicle selected to represent all vehicles on the highway in order to establish geometric standards of the highway
-largest that is likely to use the highway with considerable frequency
Guidelines in the selection of design vehicle

- Passenger car is selected when the parking lot or series of parking lots are the main traffic generators
- A single unit truck maybe chosen for the design of intersections at local streets and park roads
- A city transit bus maybe selected for the design of intersections of state highways and city streets that serve buses with relatively few large trucks
- Either an 84-passenger larger school bus 12.20 m long or a 65 -passenger conventional bus 10.98 m long may be selected

The minimum size of the design vehicle should be WB-20 at intersection of freeway ramp terminals and arterial crossroads and at intersection s of state highways and industrialized streets that carry high volumes of traffic.

## ACRONYMS

AADT- Annual average daily traffic
ADT- Average Daily Traffic
CBR- California Bearing Ratio
DHV- Design hourly volume
"Cross section elements" is on page 680 of reference text.

## Design of Flexible Pavement

$E S A L_{i}=f_{d} \times G_{j t} \times A A D T_{i} \times 365 \times N_{i} \times F_{E i}$
$=$ equivalent accumulated $18,000 \mathrm{lb}(80 \mathrm{kN})$ single-axle load for the axle category i
$f_{d}=$ design lane factor
$\mathrm{G}_{\mathrm{jt}}=$ growth factor for a given growth rate j and design period t
$A A D T_{i}=$ first year annual average daily traffic for axle category $i$
$N_{i}=$ number of axles on each vehicle in category $i$
$\mathrm{F}_{\mathrm{Ei}}=$ load equivalency factor for axle category i

Excerpt from Table 20.3 p 965 Load Equivalency Factors

| Gross Axle Load |  | Load Equivalency Factors |  |  |  |
| :--- | :--- | :--- | :---: | :---: | :---: |
|  | lb |  |  |  | For Single Axles |
| 4.45 | 1000 | 0.00002 |  |  |  |
| 8.9 | 2000 | 0.00018 |  |  |  |
| 17.8 | 4000 | 0.00209 |  |  |  |
| 26.7 | 6000 | 0.01043 |  |  |  |
| 35.6 | 8000 | 0.0343 |  |  |  |
| 44.5 | 10000 | 0.0877 |  |  |  |
| 53.4 | 12000 | 0.189 |  |  |  |

For design lane factor see Table 20.7
Table 20.7 p 970 Percentage of Total Truck Traffic on Design Lane

| Number of Traffic Lanes | Percentage of Trucks in Design Lane |
| :---: | :---: |
| 2 | 50 |
| 4 | $45(35-48)$ |
| 6 or more | $40(25-48)$ |
|  |  |

For growth factor for given growth rate and design period see Table 20.6
Excerpt of Table 20.6 p 970 Growth Factors

| Design Period, <br> years $(\mathrm{n})$ | Annual Growth Rate, Percent $(\mathrm{r})$ |  |  |
| :---: | :---: | :---: | :---: |
|  | No Growth | 2 | 4 |
| 15 | 15 | 17.29 | 20.02 |
| 20 | 20 | 24.30 | 29.78 |
| 25 | 25 | 32.03 | 41.65 |
| 30 | 30 | 40.57 | 56.08 |
| 35 | 35 | 49.99 | 73.65 |

## Example pp 971

An eight lane divided highway is to be constructed on a new alignment. Traffic volume forecasts indicate that the average annual daily traffic (AADT) in both
directions during the first year of operation will be 12,000, with the following vehicle mix and axle loads.

Passenger cars ( $1000 \mathrm{lb} /$ axle ) $=50$ percent
2-axle single unit trucks ( $6000 \mathrm{lb} /$ axle ) $=33$ percent
3 - axle single unit trucks ( $10000 \mathrm{lb} /$ axle ) $=17$ percent
The vehicle mix is expected to remain the same throughout the design life of the pavement. If the expected annual traffic growth rate is 4 percent for all vehicles, determine the design ESAL, given a design period of 20 years.
Growth factor $=29.78$
Percent truck volume on design lane $=45$
$=$ Design lane factor (in decimal equivalence)
Load Equivalency factors
Passenger cars ( 1000 lb per axle) $=0.00002$ (negligible)
2-axle single unit trucks ( $6000 \mathrm{lb} /$ axle ) $=0.01043$
3 -axle single unit trucks ( $10000 \mathrm{lb} /$ axle $)=0.0877$

## Solution

ESAL for
2 axle single unit trucks

$$
=0.45(29.78)(12,000)(365)(.33)(2)(0.01043)
$$

$$
=0.4041 \times 10^{6}
$$

ESAL for

$$
3 \text { axle single unit trucks }
$$

$=0.45(29.78)(12000)(365)(0.17)(3)(0.0877)$
$=2.6253 \times 10^{6}$
ESAL for passenger cars = negligible

Total ESAL $=3.0294 \times 10^{6}$

Main engineering property required of subgrade is resilient modulus. When resilient modulus is less than $30,000 \mathrm{lb} / \mathrm{in}^{2}$, the relationship between CBR and $\mathrm{M}_{\mathrm{r}}$ (equivalent resilient modulus ) is
$\mathrm{M}_{\mathrm{r}}$ in MPa
$=10.342 \mathrm{CBR}$

When resilient modulus is of higher value, direct measurement is recommended.

## Example

A full depth asphalt pavement is to be constructed to carry an ESAL of 2,172,042. If the subgrade 's CBR is 10 and the Mean Annual Air Temperature (MAAT) is $60^{\circ} \mathrm{F}$, determine the depth required for the asphalt layer.

$$
\begin{aligned}
\mathrm{M}_{\mathrm{r}} & =10.342 \mathrm{CBR} \\
& =10.342(10) \\
& =103.42 \mathrm{MPa} \text { or } 15,000 \mathrm{psi} \\
\text { ESAL } & =2.172042 \times 10^{6}
\end{aligned}
$$

Using the graphical way of determining thickness (using Figure 20.5, p 976), depth required for full depth asphalt layer is 22.86 cm ( 9 inches).

## Design of Rigid Pavement

## Equations developed by Westergaard

For different loading conditions

1. Edge loading when the edges of the slab are warp upward at night

$$
\sigma_{e}=(0.572 \mathrm{P}) / h^{2}\left[4 \log _{10}(/ / \mathrm{b})+\log _{10} \mathrm{~b}\right]
$$

2. Edge loading when the slab is unwarped or when the edge of the slab is curled downward in the daytime

$$
\sigma_{\mathrm{e}}=(0.572 \mathrm{P}) / \mathrm{h}^{2}\left[4 \log _{10}(/ / \mathrm{b})+0.359\right]
$$

3. Interior loading

$$
\sigma_{i}=(0.316 \mathrm{P}) / \mathrm{h}^{2}\left[4 \log _{10}(/ / \mathrm{b})+1.069\right]
$$

Where
$\sigma_{\mathrm{e}}=$ maximum stress (in psi) induced in the bottom of the slab, directly under the load P and applied at the edge and in a direction parallel to the edge
$\sigma_{i}=$ maximum tensile stress (in psi) induced at the bottom of the slab directly under the load P applied at the interior of the slab
$P=$ applied load (in pounds), including allowance for impact
$\mathrm{h}=$ thickness of slab (in inches)
| = radius of relative stiffness $=\left\{E_{c} h^{3} /\left[12\left(1-\mu^{2}\right) k\right]\right\}^{1 / 4}$
$\mathrm{E}_{\mathrm{c}}=$ modulus of elasticity of concrete (in psi)
$\mu=$ Poisson ratio of concrete $=0.15$
$\mathrm{k}=$ subgrade modulus (in lb/in. ${ }^{3}$ )
$\mathrm{b}=$ radius of equivalent distribution of pressure (in inches)
$=\left(1.6 \mathrm{a}^{2}+\mathrm{h}^{2}\right)^{1 / 2}-0.675 \mathrm{~h}$ (for $\mathrm{a}<1.724 \mathrm{~h}$ )
$=\mathrm{a}($ for $\mathrm{a}>1.724 \mathrm{~h})$
$\mathrm{a}=$ radius of contact area of load (in inches) (Contact area is usually assumed as circular for interior and corner loadings and semicircular for edge loading).

## Problem solving

Example 21.1 p 1029
Determine the tensile stress imposed by a semicircular wheel load of 900 lb imposed during the day and located at the edge of the concrete pavement with the following dimensions and properties by using the Westergaard equations.

Pavement thickness $=6$ in.
$\mu=0.15$
$\mathrm{E}_{\mathrm{c}}=5 \times 10^{6} \mathrm{lb} / \mathrm{in} .{ }^{2}$
$\mathrm{k}=130 \mathrm{lb} / \mathrm{in} .^{3}$
radius of loaded area $=3$ in.

Solution
$a<1.724 \mathrm{~h}$, then with $\mathrm{h}=6 \mathrm{in}$.
$b=\left(1.6 a^{2}+h^{2}\right)^{1 / 2}-0.675 h$
$=\left[(1.6)\left(3^{2}\right)+6^{2}\right]^{1 / 2}-0.675(6)$
$=3.05 \mathrm{in}$.

$$
\begin{aligned}
I & =\left\{E_{c} h^{3} /\left[12\left(1-\mu^{2}\right) \mathrm{k}\right]\right\}^{1 / 4} \\
& =\left\{5 \times 10^{6}(6)^{3} /\left[12\left(1-0.15^{2}\right) 130\right]\right\}^{1 / 4} \\
& =29.0 \mathrm{in} .
\end{aligned}
$$

$$
\begin{aligned}
\sigma_{\mathrm{e}} & =(0.572 \mathrm{P}) / \mathrm{h}^{2}\left[4 \log _{10}(/ / \mathrm{b})+0.359\right] \\
& =[(0.572)(900)] /(6)^{2}\left[4 \log _{10}(29 / 3.05)+0.359\right] \\
& =61.07 \mathrm{lb} / \mathrm{in}^{2}
\end{aligned}
$$

## Reference

Garber,N \& Hoel, L. (2002). Traffic and Highway Engineering (3 ${ }^{\text {rd }} \mathrm{ed}$ ). California: Thomson Learning Inc.

